



## AISI 304 MSS SP-114 CL1000 Stainless Steel Cast Threaded Hexagon Reducing Nipple

Our Product Introduction

### Basic Information

- Place of Origin: CHINA
- Brand Name: KASUGAI
- Certification: ISO-9001; PED; AD 2000
- Model Number: AISI 304 MSS SP-114 CL1000 Stainless Steel Cast Threaded Hexagon Reducing Nipple
- Minimum Order Quantity: TO BE NEGOTIATED
- Price: PER BASE MATERIAL PRICE
- Packaging Details: SEAWORTHY PACKING
- Delivery Time: 60 DAYS FOR ONE CONTAINER
- Payment Terms: L / C , T / T
- Supply Ability: 100 TONS / MONTH



### Product Specification

- Product Name: AISI 304 MSS SP-114 CL1000 1¼" X 1" Stainless Steel Cast Threaded Hexagon Reducing Nipple
- Size Range: 1/4" To 4"
- Thread Type: ASME B1.20.1(NPT), BS 21 (NSPT), DIN2999/259
- Pressure Class: Class 1000 NPT
- Standards: AISI 304/L
- Dimensions: MSS SP-114-2018
- Highlight: **Cast Threaded Hexagon Reducing Nipple, CL1000 Hexagon Reducing Nipple**

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## Product Description

### AISI 304 MSS SP-114 CL1000 Stainless Steel Cast Threaded Hexagon Reducing Nipple

#### Product Information

Product Name	AISI 304 MSS SP-114 CL1000 Stainless Steel Cast Threaded Hexagon Reducing Nipple
Thread Types	ASME B1.20.1(NPT)
Dimensions	MSS SP-114-2018
Size Range	1/4" x 1"
Pressure Class	Class 1000 NPT
Materials	AISI 304/L

#### Standard & Materials: AISI 304L

The SAE/ANSI 304 (AISI 304) is the most commonly available and used type of stainless steel. It is also referred to as 18/8 stainless steel, A2 stainless steel (as per the ISO 3506), or 304S15 (as per the British Standard). This is an austenitic chromium-nickel alloy which practically means that it has a very high corrosion resistance. It is also nonmagnetic and can't be hardened through heat treatment. As AISI 304 can withstand extremely corrosive environments and can be shaped, machined and welded relatively easy, it is very popular for a wide range of applications.

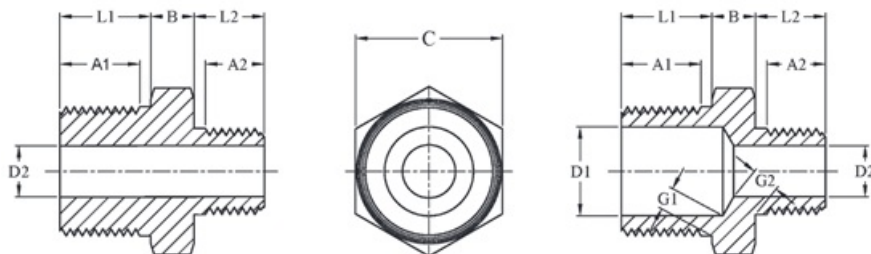
#### AISI 304/L Chemical Composition (%)

Grade	C, max	Cr	Mn, max	Ni	P, max	S, max	Si, max
AISI 304	0.08	18~20	2	8~10.5	0.045	0.03	1
AISI 304L	0.03	18~20	2	8~12	0.045	0.03	1

#### AISI 304/L Mechanical Properties

Mechanical Properties	304	304L
Hardness, Knoop	138	158
Hardness, Rockwell B	70	82
Hardness, Vickers	129	159
Tensile Strength, Ultimate	505 MPa	564 MPa
Tensile Strength, Yield	215 MPa	210 MPa
Elongation at Break	70%	58%
Modulus of Elasticity	193~200 GPa	193~200 GPa
Charpy Impact	325 J	216J

#### MSS SP-114 Dimensions of Class 1000 Wrought Hexagonal Reducing Nipples (mm)



ALTERNATE DESIGN

NPS	Thread Length (min.)	Thread Length (min.)	Length of Hex. (min.)	Length of Hex. (min.)	Nominal Flat Width	Nominal Width Across Flats (b)	Bore Dia. (max.)	Bore Dia. (max.)	Metal Thickness (min.)	Metal Thickness (min.)
	A1	A2	L1	L2	B	C	D1	D2	G1	G2
1/4 x 1/8	0.46	0.31	0.53	0.37	0.25	5/8	0.30	0.21	0.27	0.22
3/8 x 1/8	0.47	0.31	0.54	0.37	0.31	11/16 <sup>(a)</sup>	0.42	0.21	0.28	0.22
3/8 x 1/4	0.47	0.46	0.54	0.53	0.31	11/16 <sup>(a)</sup>	0.42	0.30	0.28	0.27
1/2 x 1/8	0.61	0.31	0.69	0.37	0.31	7/8	0.52	0.21	0.33	0.22
1/2 x 1/4	0.61	0.46	0.69	0.53	0.31	7/8	0.52	0.30	0.33	0.27
1/2 x 3/8	0.61	0.47	0.69	0.54	0.31	7/8	0.52	0.42	0.33	0.28
3/4 x 1/8	0.62	0.31	0.70	0.37	0.38	1 1/16 <sup>(a)</sup>	0.74	0.21	0.34	0.22
3/4 x 1/4	0.62	0.46	0.70	0.53	0.38	1 1/16 <sup>(a)</sup>	0.74	0.30	0.34	0.27
3/4 x 3/8	0.62	0.47	0.70	0.54	0.38	1 1/16 <sup>(a)</sup>	0.74	0.42	0.34	0.28

$\frac{3}{4} \times \frac{1}{2}$	0.62	0.61	0.70	0.69	0.38	$\frac{1}{16}$ (a)	0.74	0.54	0.34	0.33
$1 \times \frac{1}{8}$	0.77	0.31	0.86	0.37	0.38	$\frac{1}{8}$	0.96	0.21	0.39	0.22
$1 \times \frac{1}{4}$	0.77	0.46	0.86	0.53	0.38	$\frac{1}{8}$	0.96	0.30	0.39	0.27
$1 \times \frac{3}{8}$	0.77	0.47	0.86	0.54	0.38	$\frac{1}{8}$	0.96	0.42	0.39	0.28
$1 \times \frac{1}{2}$	0.77	0.61	0.86	0.69	0.38	$\frac{1}{8}$	0.96	0.54	0.39	0.33
$1 \times \frac{3}{4}$	0.77	0.62	0.86	0.70	0.38	$\frac{1}{8}$	0.96	0.74	0.39	0.34
$1\frac{1}{4} \times \frac{1}{4}$	0.80	0.46	0.89	0.53	0.56	$\frac{1}{4}$	1.28	0.30	0.42	0.27
$1\frac{1}{4} \times \frac{3}{8}$	0.80	0.47	0.89	0.54	0.56	$\frac{1}{4}$	1.28	0.42	0.42	0.28
$1\frac{1}{4} \times \frac{1}{2}$	0.80	0.61	0.89	0.69	0.56	$\frac{1}{4}$	1.28	0.54	0.42	0.33
$1\frac{1}{4} \times \frac{3}{4}$	0.80	0.62	0.89	0.70	0.56	$\frac{1}{4}$	1.28	0.74	0.42	0.34
$1\frac{1}{4} \times 1$	0.80	0.77	0.89	0.86	0.56	$\frac{1}{4}$	1.28	0.96	0.42	0.39
$1\frac{1}{2} \times \frac{1}{4}$	0.81	0.46	0.90	0.53	0.62	2	1.50	0.30	0.44	0.27
$1\frac{1}{2} \times \frac{3}{8}$	0.81	0.47	0.90	0.54	0.62	2	1.50	0.42	0.44	0.28
$1\frac{1}{2} \times \frac{1}{2}$	0.81	0.61	0.90	0.69	0.62	2	1.50	0.54	0.44	0.33
$1\frac{1}{2} \times \frac{3}{4}$	0.81	0.62	0.90	0.70	0.62	2	1.50	0.74	0.44	0.34
$1\frac{1}{2} \times 1$	0.81	0.77	0.90	0.86	0.62	2	1.50	0.96	0.44	0.39
$1\frac{1}{2} \times 1\frac{1}{4}$	0.81	0.80	0.90	0.89	0.62	2	1.50	1.28	0.44	0.42
$2 \times \frac{1}{4}$	0.84	0.46	0.93	0.53	0.69	$2\frac{1}{2}$	1.94	0.30	0.47	0.27
$2 \times \frac{3}{8}$	0.84	0.47	0.93	0.54	0.69	$2\frac{1}{2}$	1.94	0.42	0.47	0.28
$2 \times \frac{1}{2}$	0.84	0.61	0.93	0.69	0.69	$2\frac{1}{2}$	1.94	0.54	0.47	0.33
$2 \times \frac{3}{4}$	0.84	0.62	0.93	0.70	0.69	$2\frac{1}{2}$	1.94	0.74	0.47	0.34
$2 \times 1$	0.84	0.77	0.93	0.86	0.69	$2\frac{1}{2}$	1.94	0.96	0.47	0.39
$2 \times 1\frac{1}{4}$	0.84	0.80	0.93	0.89	0.69	$2\frac{1}{2}$	1.94	1.28	0.53	0.42
$2 \times 1\frac{1}{2}$	0.84	0.81	0.93	0.90	0.69	$2\frac{1}{2}$	1.94	1.50	0.53	0.44
$2\frac{1}{2} \times \frac{1}{2}$	1.27	0.61	1.35	0.69	0.75	3	2.40	0.54	0.53	0.33
$2\frac{1}{2} \times \frac{3}{4}$	1.27	0.62	1.35	0.70	0.75	3	2.40	0.74	0.53	0.34
$2\frac{1}{2} \times 1$	1.27	0.77	1.35	0.86	0.75	3	2.40	0.96	0.53	0.39
$2\frac{1}{2} \times 1\frac{1}{4}$	1.27	0.80	1.35	0.89	0.75	3	2.40	1.28	0.53	0.42
$2\frac{1}{2} \times 1\frac{1}{2}$	1.27	0.81	1.35	0.90	0.75	3	2.40	1.50	0.53	0.44
$2\frac{1}{2} \times 2$	1.27	0.84	1.35	0.93	0.75	3	2.40	1.94	0.53	0.47
$3 \times \frac{1}{2}$	1.33	0.61	1.42	0.69	0.81	$3\frac{1}{2}$	2.95	0.54	0.60	0.33
$3 \times \frac{3}{4}$	1.33	0.62	1.42	0.70	0.81	$3\frac{1}{2}$	2.95	0.74	0.60	0.34
$3 \times 1$	1.33	0.77	1.42	0.86	0.81	$3\frac{1}{2}$	2.95	0.96	0.60	0.39
$3 \times 1\frac{1}{4}$	1.33	0.80	1.42	0.89	0.81	$3\frac{1}{2}$	2.95	1.28	0.60	0.42
$3 \times 1\frac{1}{2}$	1.33	0.81	1.42	0.90	0.81	$3\frac{1}{2}$	2.95	1.50	0.60	0.44
$3 \times 2$	1.33	0.84	1.42	0.93	0.81	$3\frac{1}{2}$	2.95	1.94	0.60	0.47
$3 \times 2\frac{1}{2}$	1.33	1.27	1.42	1.35	0.81	$3\frac{1}{2}$	2.95	2.40	0.60	0.53
$4 \times 1$	1.43	0.77	1.52	0.86	1.00	$4\frac{5}{8}$	3.82	0.96	0.73	0.39
$4 \times 1\frac{1}{4}$	1.43	0.80	1.52	0.89	1.00	$4\frac{5}{8}$	3.82	1.28	0.73	0.42
$4 \times 1\frac{1}{2}$	1.43	0.81	1.52	0.90	1.00	$4\frac{5}{8}$	3.82	1.50	0.73	0.44
$4 \times 2$	1.43	0.84	1.52	0.93	1.00	$4\frac{5}{8}$	3.82	1.94	0.73	0.47
$4 \times 2\frac{1}{2}$	1.43	1.27	1.52	1.35	1.00	$4\frac{5}{8}$	3.82	2.40	0.73	0.53
$4 \times 3$	1.43	1.33	1.52	1.42	1.00	$4\frac{5}{8}$	3.82	2.95	0.73	0.60

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